

98 Rec'd PCT/PTO 26 NOV 2001

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| FORM PTO-1390 (Modified) (REV 11-2000) | | U.S. DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE | | ATTORNEY'S DOCKET NUMBER 216272US | |
| TRANSMITTAL LETTER TO THE UNITED STATES DESIGNATED/ELECTED OFFICE (DO/EO/US) CONCERNING A FILING UNDER 35 U.S.C. 371 | | | | U.S. APPLICATION NO. (IF KNOWN, SEE 37 CFR 09/926608 | |
| | | | | | |
| INTERNATIONAL APPLICATION NO PCT/SE99/00944 | | INTERNATIONAL FILING DATE 28 MAY 1999 | | PRIORITY DATE CLAIMED NONE | |
| TITLE OF INVENTION A WIND POWER PLANT AND A METHOD FOR CONTROL | | | | | |
| APPLICANT(S) FOR DO/EO/US Mats LEIJON, et al | | | | | |
| Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information: | | | | | |
| <ol style="list-style-type: none"> 1. <input checked="" type="checkbox"/> This is a FIRST submission of items concerning a filing under 35 U.S.C. 371. 2. <input type="checkbox"/> This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371 3. <input checked="" type="checkbox"/> This is an express request to begin national examination procedures (35 U.S.C. 371(f)). The submission must include items (5), (6), (9) and (24) indicated below. 4. <input checked="" type="checkbox"/> The US has been elected by the expiration of 19 months from the priority date (Article 31) 5. <input checked="" type="checkbox"/> A copy of the International Application as filed (35 U.S.C. 371 (c) (2)) <ol style="list-style-type: none"> a. <input type="checkbox"/> is attached hereto (required only if not communicated by the International Bureau). b. <input checked="" type="checkbox"/> has been communicated by the International Bureau. c. <input type="checkbox"/> is not required, as the application was filed in the United States Receiving Office (RO/US). 6. <input checked="" type="checkbox"/> An English language translation of the International Application as filed (35 U.S.C. 371(c)(2)) <ol style="list-style-type: none"> a. <input checked="" type="checkbox"/> is attached hereto. b. <input type="checkbox"/> has been previously submitted under 35 U.S.C. 154(d)(4). 7. <input checked="" type="checkbox"/> Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371 (c)(3)) <ol style="list-style-type: none"> a. <input type="checkbox"/> are attached hereto (required only if not communicated by the International Bureau). b. <input type="checkbox"/> have been communicated by the International Bureau. c. <input type="checkbox"/> have not been made; however, the time limit for making such amendments has NOT expired. d. <input checked="" type="checkbox"/> have not been made and will not be made. 8. <input type="checkbox"/> An English language translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)). 9. <input type="checkbox"/> An oath or declaration of the inventor(s) (35 U.S.C. 371 (c)(4)). 10. <input type="checkbox"/> An English language translation of the annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371 (c)(5)). 11. <input type="checkbox"/> A copy of the International Preliminary Examination Report (PCT/IPEA/409). 12. <input checked="" type="checkbox"/> A copy of the International Search Report (PCT/ISA/210). <p>Items 13 to 20 below concern document(s) or information included:</p> <ol style="list-style-type: none"> 13. <input type="checkbox"/> An Information Disclosure Statement under 37 CFR 1.97 and 1.98. 14. <input type="checkbox"/> An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included. 15. <input checked="" type="checkbox"/> A FIRST preliminary amendment. 16. <input type="checkbox"/> A SECOND or SUBSEQUENT preliminary amendment 17. <input type="checkbox"/> A substitute specification 18. <input type="checkbox"/> A change of power of attorney and/or address letter. 19. <input type="checkbox"/> A computer-readable form of the sequence listing in accordance with PCT Rule 13ter.2 and 35 U.S.C. 1.821 - 1.825. 20. <input type="checkbox"/> A second copy of the published international application under 35 U.S.C. 154(d)(4). 21. <input type="checkbox"/> A second copy of the English language translation of the international application under 35 U.S.C. 154(d)(4). 22. <input type="checkbox"/> Certificate of Mailing by Express Mail 23. <input checked="" type="checkbox"/> Other items or information <p>Drawings (6 sheets) Request for Consideration of Documents Cited in the International Search Report</p> | | | | | |

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| U.S. APPLICATION NO (IF KNOWN, SEE 37 CFR 1.53) 09/926608 | | INTERNATIONAL APPLICATION NO PCT/SE99/00944 | | ATTORNEY'S DOCKET NUMBER 216272US | |
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24. The following fees are submitted:

| BASIC NATIONAL FEE (37 CFR 1.492 (a) (1) - (5)) : | | | | CALCULATIONS PTO USE ONLY | |
|---|---|--------------|-----------|---------------------------|--|
| <input checked="" type="checkbox"/> | Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO | \$1040.00 | | | |
| <input type="checkbox"/> | International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO | \$890.00 | | | |
| <input type="checkbox"/> | International preliminary examination fee (37 CFR 1.482) not paid to USPTO but international search fee (37 CFR 1.445(a)(2)) paid to USPTO | \$740.00 | | | |
| <input type="checkbox"/> | International preliminary examination fee (37 CFR 1.482) paid to USPTO but all claims did not satisfy provisions of PCT Article 33(1)-(4) | \$710.00 | | | |
| <input type="checkbox"/> | International preliminary examination fee (37 CFR 1.482) paid to USPTO and all claims satisfied provisions of PCT Article 33(1)-(4) | \$100.00 | | | |
| ENTER APPROPRIATE BASIC FEE AMOUNT = | | | | \$1,040.00 | |
| Surcharge of \$130.00 for furnishing the oath or declaration later than months from the earliest claimed priority date (37 CFR 1.492 (e)). <input type="checkbox"/> 20 <input checked="" type="checkbox"/> 30 | | | | \$130.00 | |
| CLAIMS | NUMBER FILED | NUMBER EXTRA | RATE | | |
| Total claims | 38 - 20 = | 18 | x \$18 00 | \$324.00 | |
| Independent claims | 3 - 3 = | 0 | x \$84.00 | \$0.00 | |
| Multiple Dependent Claims (check if applicable). <input type="checkbox"/> | | | | \$0.00 | |
| TOTAL OF ABOVE CALCULATIONS = | | | | \$1,494.00 | |
| <input type="checkbox"/> Applicant claims small entity status. See 37 CFR 1.27. The fees indicated above are reduced by 1/2. | | | | \$0.00 | |
| SUBTOTAL = | | | | \$1,494.00 | |
| Processing fee of \$130.00 for furnishing the English translation later than months from the earliest claimed priority date (37 CFR 1.492 (f)). <input type="checkbox"/> 20 <input type="checkbox"/> 30 + | | | | \$0.00 | |
| TOTAL NATIONAL FEE = | | | | \$1,494.00 | |
| Fee for recording the enclosed assignment (37 CFR 1.21(h)). The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31) (check if applicable). <input type="checkbox"/> | | | | \$0.00 | |
| TOTAL FEES ENCLOSED = | | | | \$1,494.00 | |
| | | | | Amount to be: refunded \$ | |
| | | | | charged \$ | |

a. ☒ A check in the amount of \$1,494.00 to cover the above fees is enclosed.


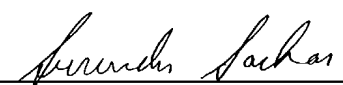
b. ☐ Please charge my Deposit Account No. _____ in the amount of _____ to cover the above fees. A duplicate copy of this sheet is enclosed.

c. ☒ The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. 15-0030 A duplicate copy of this sheet is enclosed

d. ☐ Fees are to be charged to a credit card. **WARNING:** Information on this form may become public. **Credit card information should not be included on this form.** Provide credit card information and authorization on PTO-2038

NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137(a) or (b)) must be filed and granted to restore the application to pending status.

SEND ALL CORRESPONDENCE TO.

| | |
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| Telephone #: (703) 413-3000 Facsimile #: (703) 413-2220 <div style="text-align: center;">  22850 </div> | <div style="text-align: right;">  SIGNATURE Gregory J. Maier NAME 25,599 REGISTRATION NUMBER <u>Nov. 26 2001</u> DATE </div> |
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216272US-234271-9847-6X PCT
ENKEL 8634

IN THE UNITED STATES PATENT & TRADEMARK OFFICE

IN RE APPLICATION OF :
Mats LEIJON :
SERIAL NO: NEW APPLICATION : ATTN: APPLICATION DIVISION
(Based on PCT/SE99/00944)
FILED: HERewith
FOR: A WIND POWER PLANT AND
A METHOD FOR CONTROL

PRELIMINARY AMENDMENT

ASSISTANT COMMISSIONER FOR PATENTS
WASHINGTON, D.C. 20231

SIR:

Prior to examination on the merits, please amend the above-identified application
as follows:

IN THE SPECIFICATION

Page 15, beginning at line 21, delete the paragraph and insert the following
paragraph:

In the variant according to Fig 5. it is illustrated how a transformer 38 common
for the generators 1, is arranged between the parallel connection point 35 for the
generators 1 and the frequency converter 34, which transformer is intended to achieve a
high voltage in the part of the connection situated between the transformer and the
frequency converter 34 and a comparatively lower voltage between said transformer 38

and the generators 1 . This common transformer 38 is located on the wind power side of the connection 30, i.e. close to the wind power station 29, so that the main part of the connection 30 will be present between the transformer 38 and the frequency converter 34. Suitably the transformer 38 can be placed on one of the foundations for the wind power stations 29 or possibly on its own foundation on a strategic place.

IN THE CLAIMS

Please cancel Claims 1-34.

Please add new Claims 35-72 as follows:

35. (New) A wind power plant, comprising:

a wind power station having a wind turbine and an electric generator; and
an electric alternating voltage connection between the wind power station and at

least one of an external transmission network and an external distribution network,

said electric alternating voltage connection including a frequency converter arranged on network side of the wind power plant and configured to fix a station frequency substantially below a network frequency of at least one of the external transmission network and the external distribution network, and to convert the frequency of the electric alternating voltage connection to match the network frequency.

36. (New) A wind power plant according to claim 35, wherein:

the frequency converter is configured to vary the frequency of the alternating voltage connection and a voltage of the electric alternating voltage connection.

37. (New) A wind power plant according to claim 35, wherein:

the frequency converter is configured to fix the station frequency to 20Hz or lower.

38. (New) A wind power plant according to claim 37, wherein:
the frequency converter is configured to fix the station frequency within an inclusive range of 2-20 Hz.

39. (New) A wind power plant according to claim 35, wherein:
the frequency converter is configured to fix the voltage of the electric alternating voltage connection within an inclusive range of 10-400 kV.

40. (New) A wind power plant according to claim 35, wherein:
the frequency converter comprises a direct voltage intermediate link having an AC/DC converter, and an inverter having an alternating voltage side and a direct voltage side.

41. (New) A wind power plant according to claim 40, wherein:
the direct voltage intermediate link comprises a DC/DC converter.

42. (New) A wind power plant according to claim 40, wherein:
the inverter is configured to be a voltage stiff self-commutated inverter.

43. (New) A wind power plant according to claim 40, further comprising:
a capacitor connected in parallel to the inverter on the direct voltage side of the inverter.

44. (New) A wind power plant according to claim 40, further comprising:
a plurality of network inductances connected in series with each phase of the alternating voltage side of the inverter.

45. (New) A wind power plant according to claim 35, wherein:
the frequency converter comprises a plurality of insulated gate bipolar transistor valves connected in series.

46. (New) A wind power plant according to claim 35, further comprising

at least one other wind power station, wherein the wind power station and the at least one other wind power station are connected in parallel.

47. (New) A wind power plant according to claim 35, wherein:
the electric generator is configured to be asynchronous.

48. (New) A wind power plant according to claim 35, wherein:
the wind turbine is connected to the electric generator via a gear mechanism.

49. (New) A wind power plant according to claim 48, wherein:
the gear mechanism comprises a single step planetary gear.

50. (New) A wind power plant according to claim 35, wherein:
the electric generator comprises at least one winding that comprises a solid insulation layer.

51. (New) A wind power plant according to claim 50, wherein:
the winding comprises an insulation system having at least two semiconducting layers, each of which essentially constitutes equipotential surfaces, and that the solid insulation layer is located between the at least two semiconducting layers.

52. (New) A wind power plant according to claim 51, wherein:
at least one of the at least two semiconducting layers is configured to have a thermal coefficient of expansion equal to a thermal coefficient of expansion of the solid insulation layer.

53. (New) A wind power plant according to claim 50, wherein:
the winding comprises a high-voltage cable.

54. (New) A wind power plant according to claim 51, wherein:

an innermost semiconducting layer of the at least two semiconducting layers is configured to have a potential essentially equal to an electric conductor.

55. (New) A wind power plant according to claim 54, wherein:
the innermost semiconducting layer of the at least two semiconducting layers is configured to be in electrical contact with at least a portion of the electric conductor.

56. (New) A wind plant according to claim 51, wherein:
an outermost semiconducting layer of the at least two semiconducting layers is connected to a node at a predetermined potential.

57. (New) A wind power plant according to claim 56, wherein:
the predetermined fixed potential is at least one of a ground potential and a low voltage potential.

58. (New) A wind power plant according to claim 35, wherein:
the wind power station comprises a step-down transformer configured to step-down the voltage between the electric generator and the frequency converter.

59. (New) A wind power plant according to claim 35, wherein:
the wind power station comprises a step-down transformer configured to step-down the voltage between the electric generator of the wind power station and the frequency converter; and

the at least one other wind power station comprises another step-down transformer configured to step-down the voltage between an electric generator of the at least one other wind power station and the frequency converter.

60. (New) A wind power plant according to claim 46, further comprising:

a common step-down transformer connected between the frequency converter and the wind power station, and between the frequency converter and the at least one other wind power station.

61. (New) A wind power plant according to claim 60, wherein:
the wind power station comprises a step-down transformer configured to have a primary side connected to the electric generator and a secondary side connected in parallel to a primary side of the common step-down transformer.

62. (New) A wind power plant according to claim 35, further comprising:
at least one of a cable configured to be submerged into water and a cable configured as an aerial line.

63. (New) A wind power plant according to claim 35, wherein:
the frequency converter comprises a frequency converter control unit configured to control a frequency at the electric alternating voltage connection.

64. (New) A wind power plant according to claim 35, further comprising:
an active power measuring unit; and

a wind speed measuring unit,

wherein the active power measuring unit and the wind speed measuring unit are configured to send control signals to the frequency converter control unit.

65. (New) A wind power plant according to claim 64, wherein:
the frequency converter control unit is configured to control the frequency at the electric alternating voltage connection with an ideal characteristic over rotational speed as a function of wind speed.

66. (New) A wind power plant according to claim 64, wherein:

the frequency converter control unit is configured to control the frequency at the electric alternating voltage connection by comparison of a measured transmitted active power with an ideal characteristic over rotational speed as a function of power.

67. (New) A wind power plant according to claim 63, wherein:
the frequency converter control unit is configured to control the frequency converter to maintain a constant voltage/frequency ratio at the electric alternating voltage connection over a predetermined major part of a predetermined frequency range.

68. (New) A method for controlling an operation of a wind power plant comprising steps of:

fixing an electric frequency output by the wind power station to a frequency substantially below a network frequency, said wind power plant having a wind power station with a wind turbine and an electric generator having a cable comprised of a flexible electric conductor, an inner semiconductor layer, an insulation layer and an outer semiconductor layer, and

an alternating current connection connecting the wind power plant with at least one of a transmission network and a distribution network; and

converting the electric frequency output by the wind power station to match the network frequency.

69. (New) A method for controlling the operation of a wind power plant according to claim 68, further comprising steps of:

comparing a measured wind speed with an ideal over rotational speed as a function of wind speed to determine a frequency converter control value; and

regulating the frequency of the alternating current connection with the frequency converter control value.

70. (New) A method for controlling the operation of a wind power plant according to claim 68, wherein:

said regulating step includes a substep of comparing a measured active power at the alternating current connection with an ideal over rotational speed as a function of active power.

71. (New) A method for controlling the operation of a wind power plant according to claim 68, wherein:

said regulating step includes controlling the frequency of the alternating current connection to maintain a constant voltage/frequency over a predetermined major part of a predetermined frequency range.

72. (New) A wind power plant comprising:

a wind power station with a wind turbine and an electric generator having a cable comprised of a flexible electric conductor, an inner semiconductor layer, an insulation layer and an outer semiconductor layer;

an alternating current connection connecting the wind power plant with at least one of a transmission network and a distribution network;

means for fixing an electric frequency output by the wind power station to a frequency substantially below a network frequency; and

means for converting the frequency output by the wind power station to match the network frequency.

REMARKS

Favorable consideration of this Application as presently amended is respectfully requested.

Claims 35-72 are active in the present Application; Claims 1-34 having been canceled and Claims 35-72 added by way of the present Preliminary Amendment. The new claims have been drafted in a manner consistent with U.S. practice. It is therefore believed that no issues of new matter have been raised.

The present document is one of a set of patent applications containing related technology as was discussed in "response to petition under 37 C.F.R. §1.182 seeking special treatment relating to an electronic search tool, and decision on petition under 37 C.F.R. §1.183 seeking waiver of requirements under 37 C.F.R. §1.98," filed in the holding application (U.S. Patent Application No. 09/147,325). Consistent with this decision, a copy of the decision is filed herewith. Also, an Information Disclosure Statement is filed herewith including a PTO Form 1449 with references that are included as part of the specially-created official digest in class 174. It is believed that submission of these materials and the reference to the holding application (Serial No. 09/147,325) is sufficient for the present Examiner to consider the references in the holding application, consistent with the decision.

Accordingly, examination on the merits of Claims 35-72 is believed to be in order, and an early and favorable action is respectfully requested.

Respectfully submitted,

OBLON, SPIVAK, McCLELLAND,
MAIER & NEUSTADT, P.C.



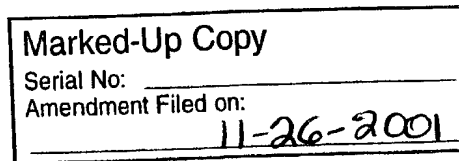
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IN THE SPECIFICATION

Page 15, beginning at line 21, delete the paragraph and insert the following paragraph:

In the variant according to Fig 5. it is illustrated how a transformer [32] 38 common for the generators 1, is arranged between the parallel connection point 35 for the generators 1 and the frequency converter 34, which transformer is intended to achieve a high voltage in the part of the connection situated between the transformer and the frequency converter 34 and a comparatively lower voltage between said transformer 38 and the generators 1. This common transformer 38 is located on the wind power side of the connection 30, i.e. close to the wind power station 29[.] , so that the main part of the connection 30 will be present between the transformer 38 and the frequency converter 34. Suitably the transformer 38 can be placed on one of the foundations for the wind power stations 29 or possibly on its own foundation on a strategic place.

IN THE CLAIMS

Claims 1-34 (Canceled).

Claims 35-72 (New).

6/pst

5

10 **A WIND POWER PLANT AND A METHOD FOR
CONTROL****FIELD OF THE INVENTION**

15 This invention relates to a wind power plant comprising at least one wind power station, which includes a wind turbine, an electric generator driven by this wind turbine, and an electric alternating voltage connection connecting the wind power station with a transmission network or distribution network. The invention also relates to a method for control in such a wind power
20 plant.

The invention is preferably intended to be used in such cases where the connection between the generator and the transmission or distribution network includes a cable intended to be
25 submerged into water. Consequently, expressed in other words, it primarily relates to such applications where one or several wind turbines with associated generators are intended to be placed in seas or lakes, wherein the cable connection extends to the transmission or distribution network placed on land. Even
30 though the advantages of the invention in the following primarily will be dealt with in connection with location of the wind turbines in seas or lakes, the invention can, however, also imply advantages in cases where the wind turbines and the generators are located on land and the connection, which in that case not necessarily has to consist of a cable but instead can be realized in
35 the form of aerial lines or cables, connects several such wind

turbines/generators with the transmission or distribution network.

BACKGROUND OF THE INVENTION AND PRIOR ART

5 When locating wind power at sea it is required, in order to get economy in the project, that large groups of wind power stations are being located within a limited area. Sea based wind power requires relatively large wind power stations (3MW and above)
10 and a suitable total system power of 50-100 MW is expected. So far the planning of such wind parks has presupposed that the electrical power transmission is effected by traditional alternating current transmission in three-phase alternating voltage sea cable systems. In that case, the generator is almost always a
15 three-phase asynchronous generator. It is true that there are examples where synchronous generators have been used directly connected to the network, but this has as a rule resulted in that a complicated mechanical spring suspension has had to be installed between the generator and the engine house in order
20 to dampen power variations caused by the varying character of the wind load. This depends on the fact that the rotor dynamics of a synchronous generator mechanically behaves like a spring against a stiff alternating voltage network, whereas an asynchronous generator behaves like a damper. A conventional
25 asynchronous generator of 3 MW could presumably be made for about 3-6 kV and be connected in series with a transformer which steps up the voltage to, let us say 24 kV, in a first step. In a wind power park with 30-40 wind power stations there would then be provided a central transformer which further steps up
30 the voltage to 130 kV. The advantage with such a system is that it is cheap and does not require any complicated sub-systems. The disadvantage partly lies in the difficulties to technically transmit power over long distances in a high-voltage alternating voltage cable. This depends on the fact that the cable produces
35 capacitive reactive power, which increases with the length. The current through the conductor and in the cable shield then in-

creases so much that the cable cannot be realized for long distances. The other disadvantage lies in that the varying wind load causes voltage variations on the transmission line, which could affect the power consumers that are connected nearby. This applies in particular if the network is "weak", i.e. has a low short-circuiting power. Due to the abovementioned technical problems with long cable transmission distances, one might be forced to connect the wind park to a "weak" network. According to certain guiding principles, the voltage variation may not be more than 4%. Different countries have different regulations and as a rule the regulations are mitigated in case of a lower voltage level on the transmission line. Voltage variations could also have to be treated differently depending on time intervals. Rapid voltage variations causes "flicker", i.e. light variations in glow lamps, which is regulated in rules.

A solution, lying at the side of the present invention, concerning the abovementioned problems with long cable distances is to transmit the power with high-voltage direct voltage. The cable can then be drawn right up to a strong network. Another advantage is that DC-transmissions have lower losses than AC-transmissions. From a technical point of view the cable distance can then be of unlimited length. A HVDC-link consists of a rectifier station, a transmission line (cable or aerial line), an inverter station and filters for removing overtones generated during the conversion. In an older variant of HVDC-links thyristors are used for rectification and inversion. Thyristors can be switched on but not switched off: the commutation takes place at the zero-crossing of the voltage, which is determined by the alternating voltage, and the converters are therefore called line commutating. A disadvantage with this technique is that the converters consume reactive power and cause current overtones, which are sent out in the network. In a more modern direct voltage solution, IGBT:s are used instead of thyristors in the converters. An IGBT (Insulated Gate Bipolar Transistor) can be switched on as well as switched off and furthermore has a high switch fre-

quency. This implies that the converters can be produced according to a completely different principle. so called self-commutating converters. To sum up, the advantages with self-commutating converters are that they can deliver as well as consume reactive power, which makes possible an active compensation of the voltage level on the network side if the network is weak. Consequently, this makes this type of converter superior to the older technique in the way that it can be connected to a network being situated closer to the wind power. The high switch frequency also leads to a reduction of the problem with overtones as compared with the older generation of HVDC. A disadvantage is, however, that the losses in the converter station are higher as well as the price. A self-commutating converter is characterized in that the voltage is built up by a rapid pulse pattern, which is generated by the converter. The voltage difference between the pulse pattern and the sinusoidal network voltage will lie above the inductances on the network side. There are two types of self-commutating inverters: a voltage stiff, VSI (Voltage Source Inverter) and a current stiff, CSI (Current Source Inverter). with somewhat different characteristics. VSI, which has at least one capacitor on the DC-side, has the best power regulation.

There have been built some experimental wind power stations using technique resembling the HVDC-concept, but for a completely different reason, namely for achieving a variable rotational speed of individual wind power stations. The generator of the wind power station is then disconnected from the network via a DC-link on low voltage, typically the 400 V or 660 V level. A variable rotational speed on the turbine gives energy gains at the same time as it as a rule results in that the variations of the rotational speed can be used for eliminating the rapid power pulsations, which cause "flicker". However, it is of course not possible to eliminate the slow power changes, which are inherent in the nature of the wind load. The moment of inertia of the turbine could be said to function as an intermediate storage for

kinetic energy. In such a system a synchronous generator is not to any disadvantage, but rather to an advantage, since the asynchronous generator requires a more expensive and more complicated rectifier. If it is desired to have a direct driven generator and consequently eliminate the need of a gear unit between the turbine and the generator, the generator must be synchronous since it will be provided with so many poles. In other words, a direct driven generator requires a DC-intermediate link. In the concept it is also possible to actively regulate the moment by changing the trigger angle, if a controlled rectifier is used. In most concepts having a variable rotational speed, an external active rotational speed control is furthermore provided by so called pitch control, which implies that the blade angle is changed on the turbine. A disadvantage with a variable rotational speed according to the related concepts is the price of the required power electronics and furthermore that the maintenance of such power electronics out at sea will be difficult and costly.

20 PURPOSE OF THE INVENTION

The purpose of the present invention is to achieve, with deviation from the abovementioned direct voltage connections, an alternating voltage connection between a particularly sea based wind park and a particularly land located transmission or distribution network with the possibility of considerably longer transmission distances and lower losses than what is offered by a conventional alternating voltage connection, and at the same time create the possibility for operation with a variable rotational speed without any power electronics at all out at sea. This is very valuable, since all maintenance taking place at sea is expensive and difficult to perform. A further purpose with the invention is to achieve the same good regulation possibilities concerning reactive power as offered by a modern HVDC-system.

35

SUMMARY OF THE INVENTION

The purpose of the invention is primarily achieved in that a frequency converter is connected to the electrical alternating voltage connection on the network side of the plant, which frequency converter is arranged to fix the frequency of the connection between the wind power station and the converter to be essentially below the network frequency and to convert this low frequency of the connection into correspondence with the higher frequency of the network. The expression "on the network side of the plant" consequently means that the frequency converter is located relatively close to the transmission or distribution network, whereas the principle part of the connection extends between the frequency converter and the wind power station itself, for instance in the form of a submarine cable. Consequently, this implies that the transmission in the connection essentially will take place at a low frequency, and consequently prerequisites of considerably longer transmission distances and lower losses are created than offered by a conventional alternating voltage connection with regular network frequency. Normally occurring network frequencies are in the level from 50 to 60 Hz. If the low frequency in the alternating voltage connection between the frequency converter and the wind power station for instance is 10 Hz, the capacitive current in a cable is reduced 5 times for the same voltage as in a 50 Hz network. This implies that distances being 5 times as long can be connected with for instance a submarine cable.

A further advantage of the invention is that the frequency converter consequently will be located close to the transmission or distribution network, i.e. normally on land, which drastically reduces the costs for maintenance and supervision and also reduces the duration of service interruptions in case of breakdowns.

According to a preferred embodiment of the invention, several wind power stations with asynchronous generators are interconnected parallelly with the alternating voltage connection. The suitable frequency and voltage of the alternating voltage connection depends on the size of the wind park and the distance from land, but for a 50 MW wind park a frequency of 10-20 Hz at 130 kV should be suitable.

According to an embodiment of the invention, the frequency converter comprises a direct voltage intermediate link with an AC/DC-converter and an inverter arrangement. This makes it possible to put a variable frequency as well as a variable voltage on the low-frequency alternating voltage connection. In particular it is then preferred that a DC/DC-converter is comprised in the direct voltage intermediate link. Even though, in a preferred embodiment, valves in the frequency converter consist of IGBT:s connected in series, other types of valves would be possible to use. Also other types of frequency converters, for instance direct converters, also called "cyclo converters", which lack a direct voltage link, can be used with the invention as well as also other frequency converters than static ones, i.e. also rotary frequency converters. According to embodiments, dealt with in more detail later on, at least one transformer can be arranged on the generator side of the connection for step-down transformation of the voltage of the alternating voltage connection between the generator and the frequency converter to a suitable generator voltage level. In that case, each of the occurring generators can be provided with its own transformer, in addition to which as a complement or an alternative thereof, a transformer being common for all generators can be provided. Consequently, such transformers make it possible to increase the voltage in the alternating voltage connection to a higher level than conventional generators are capable of. A disadvantage of such transformers is that they imply an extra cost and also entail the deficiency that the total effectivity of the system is reduced. They also imply a risk of fire and a risk for the envi-

ronment since they contain transformer oil, which can leak out in case of breakdown or vandalism.

5 With the generator technology of today concerning wind power stations, it is possible to produce a generator which can handle 10 kV, but higher voltages than that would be desirable. Furthermore, the conventional insulation technology for stator windings is sensitive to temperature variations, humidity and salt, which a wind turbine generator is exposed to.

10 According to a particularly preferred embodiment of the invention, a solid insulation is used for at least one winding in the generator, which insulation preferably is performed according to the subsequent claim 14. The winding has more specifically the character of a high-voltage cable. A generator manufactured in this way, creates the prerequisites of achieving considerably higher voltages than conventional generators. Up to 400 kV can be achieved. Furthermore, such an insulation system in the winding implies insensibility to salt, humidity and temperature variations. The high output voltage implies that transformers can be completely excluded, which implies avoidance of the already mentioned disadvantages of such transformers.

25 A generator having such a winding formed by a cable can be produced by threading the cable in slots performed for this purpose in the stator, whereupon the flexibility of the winding cable implies that the threading work can be easily performed.

30 The two semiconducting layers of the insulation system have a potential compensating function and consequently reduce the risk of surface glow. The inner semiconducting layer is to be in electrically conducting contact with the electrical conductor, or a part thereof, located inwardly of the layer, in order to obtain the same potential as this. The inner layer is intimately fastened to the solid insulation located outwardly thereof and this also applies to the fastening of the outer semiconducting layer to the

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solid insulation. The outer semiconducting layer tends to contain the electrical field within the solid insulation.

- 5 In order to guarantee a maintained adherence between the semiconducting layers and the solid insulation also during temperature variations, the semiconducting layer and the solid insulation have essentially the same thermal coefficient of expansion.
- 10 The outer semiconducting layer in the insulation system is connected to ground potential or otherwise a relatively low potential.
- 15 In order to achieve a generator capable of very high voltage, the generator has a number of features which have already been mentioned above and which distinctly differ from conventional technology. Further features are defined in the dependent claims and are discussed in the following:
- 20 Features which have been mentioned above and other essential characteristics of the generator and consequently of the wind power plant according to an embodiment of the invention comprise the following:
- 25 - The winding in the magnetic circuit is produced of a cable having one or several permanently insulated electrical conductors with a semiconducting layer at the conductor and outwardly of the solid insulation. Typical cables of this kind are cables having an insulation of cross-linked polyethylene
- 30 or ethylene-propene, which for the purpose here in question are further developed concerning stands of the electrical conductor and also the character of the insulation system.
- 35 - Cables having a circular cross section are preferred, but cables having another cross section can also be used for instance in order to achieve a better packing density.

- Such a cable makes it possible to design a laminated core of the magnetic circuit in a new and optimal way as concerns slots and teeth.
- 5
- Advantageously, the winding is produced with a stepwise increasing insulation for the best utilization of the laminated core.
- 10
- Advantageously, the winding is produced as a concentric cable winding, which makes it possible to reduce the number of coil end crossings.
- 15
- The shape of the slots is adapted to the cross section of the winding cable so that the slots are in the form of a number of cylindrical openings extending axially and/or radially outwardly of each other and having constrictions running between the layers of the stator winding.
- 20
- The shape of the slots is adapted to the cable cross section in question and to the stepwise changing thickness of the insulation of the winding. The stepwise insulation makes it possible for the magnetic core to have an essentially constant tooth width independent of the radial extension.
- 25
- The abovementioned further development concerning the stands implies that the winding conductor consisting of a number of layers brought together, i.e. insulated strands, does not necessarily have to be correctly transposed, non-
- 30
- insulated and/or insulated from each other.
- 35
- The abovementioned further development concerning the outer semiconducting layer implies that the outer semiconducting layer is cut off at suitable points along the length of the cable and each cut-off partial length is directly connected to ground potential.

The use of a cable of the type described above makes it possible that the hole length of the outer semiconducting layer of the cable, as well as other parts of the plant, can be kept at ground potential. An important advantage is that the electrical field is close to zero in the coil end region outwardly of the outer semiconducting layer. With ground potential on the outer semiconducting layer the electric field does not have to be controlled. This implies that there will occur no field concentrations neither in the core, nor in the coil end regions or in the transition section between them.

The mixture of insulated and/or non-insulated strands packed together, or transposed strands, results in low eddy current losses. The cable can have an outer diameter in the order of 10-40 mm and a conductor area in the order of 10-200 mm².

Furthermore, the invention comprises a method for controlling the operation of a wind power plant according to the subsequent claims.

BRIEF DESCRIPTION OF THE DRAWINGS

With reference to the subsequent drawings, a closer description of embodiments of the invention given as examples will follow below. In the drawings:

Fig 1 is a schematic axial end view of a sector of the stator in an electric generator in the wind power plant according to the invention.

Fig 2 is an end view, partly cut, of a cable used in the stator winding according to Fig 1,

Fig 3 is a schematic view, partly in section, of an embodiment of a wind power generator according to the invention,

Fig 4 is a schematic view showing the embodiment of the wind power plant according to the invention,

- 5 Fig 5 is likewise a schematic view illustrating an alternative embodiment of the plant,

Fig 6 is a view similar to Fig 5 of a variant, and

- 10 Fig 7 is a view illustrating a possible embodiment of the frequency converter comprised in the plant.

DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

- 15 With the aid of Figs 1-3 the design of the generator 1 preferred in an embodiment of the invention is first explained. Fig 1 shows a schematic axial view through a sector of the stator 2. The rotor of the generator is denoted as 3. The stator 2 is in a conventional way formed of a laminated core. Fig 1 shows a sector of the generator corresponding to a pole pitch. From a yoke section of the core, located furthest out in radial direction, a number of teeth 5 extend radially inwards towards the rotor 3 and these teeth are separated by a slot 6, in which the stator winding is arranged. Cables 7 forming this stator winding are high-voltage cables which can be of essentially the same type as those used for power distribution, i.e. PEX-cables (PEX = cross-linked polyethylene). A difference is that the external mechanically protecting PVC-layer and the metal shield normally surrounding such a power distribution cable have been eliminated so that the cable for the present invention only comprises the electrical conductor and at least one semiconducting layer on each side of an insulating layer. The cables 7 are schematically illustrated in Fig 1, wherein only the electrically conducting central part of each cable section or coil side is shown. It appears that each slot 6 has a varying cross section with alternating broad parts 8 and narrow parts 9. The broad parts 8 are essentially circular

and surround the cable. waist sections between the broad parts forming the narrow parts 9. The waist sections serve to radially fix the position of each cable. The cross section of the slot 6 becomes narrower radially inwards. This depends on that the voltage in the cable sections are lower the closer they are situated to the radially innermost part of the stator 1. Thinner cables can therefore be used inwards, whereas thicker cables are required further out. In the illustrated example, cables with three different dimensions and arranged in three correspondingly dimensioned sections 10, 11, 12 of the slot 6 are used. A winding 13 for auxiliary power is arranged furthest out in the slot 6.

Fig 2 shows a stepwise cut end view of a high-voltage cable for use in the generator. The high-voltage cable 7 comprises one or several electrical conductors 14, each of which comprises a number of strands 15, which together give a circular cross section. The conductors can for instance be of copper. These conductors 14 are arranged in the middle of the high-voltage cable 7 and in the shown embodiment each of the conductors is surrounded by a partial insulation 16. It is however possible to omit the partial insulation 16 on one of the conductors 14. In the shown embodiment the conductors 14 are surrounded by a first semi-conducting layer 17. Around this first semiconducting layer 17 there is an insulation layer 18, e.g. of PEX-insulation, which in its turn is surrounded by a second semiconducting layer 19. Consequently, the concept "high-voltage cable" does not, in this application, have to comprise any metal shield or any external protective layer of the type normally surrounding a power distribution cable.

In Fig 3 a wind power station is shown with a magnetic circuit of the type described with reference to Figs 1 and 2. The generator 1 is driven by a wind turbine 20 via a shaft 21. Even though the generator 1 can be direct driven by the turbine 20, i.e. that the rotor of the generator is coupled fixed in rotation to the shaft of the turbine 20, there can be a gearing 22 between the turbine 20

and the generator 1. This can for instance be constituted by a single-step planetary gearing, the purpose of which is to change up the rotational speed of the generator in relation to the rotational speed of the turbine. The stator 2 of the generator carries
5 the stator windings 23, which are built up of the cable 7 described above. The cable 7 can be unsheathed and pass on into a sheathed cable 24 via a cable joint 25.

10 In Fig 4, which in a schematic form broadly illustrates the wind power plant, two wind power stations 29 connected in parallel are illustrated, each having a generator. The generator has a field winding 26 and one (or several) auxiliary power windings 27. In the shown embodiment the generators are Y-connected and the neutral point is grounded via a respective impedance
15 28.

In Fig 4 the two wind power stations, embracing generator 1 as well as (not shown) wind turbine, are generally denoted as 29. An electric alternating voltage connection 30 connects the two
20 wind power stations 29 to a transmission or distribution network 31. This is here of three-phase type. The normal frequency of such a network is 50 or 60 Hz. The connection 30 comprises, along a section denoted as 32, a cable 33 intended to be submerged into water. However, instead of a cable submerged into
25 water, one or several aerial lines/cables could also come into question. The section 32 can in practice be very large.

On the network side of the plant a frequency converter 34 is connected to the electrical alternating voltage connection 30,
30 which frequency converter is arranged to fix the frequency of the connection between the wind power station 29 and the converter 34 to be substantially below the frequency of the network 31 and to convert this low frequency of the connection into correspondence with the higher frequency of the network 31.

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As appears from the previous description, the generator 1 is of asynchronous type in the example.

5 The frequency converter 34 is suitably located on land in a suitable station nearby the network 31. The wind power stations 29 are located out at sea or a lake on suitable foundations. On one of these foundations, or on a foundation particularly set ups for this purpose, the outgoing cables from the generators 1 are interconnected, e.g. via bus-bars, in a point denoted as 35.

10

In Fig 4 it is illustrated how a circuit breaker 36 is provided between the frequency converter 34 and the network 31 and sets of disconnectors on each side thereof.

15 In the embodiment according to Fig 4 the generators 1 are direct coupled to the frequency converter 34. This is a consequence of the fact that the generators 1 are supposed to be of the design described above with reference to Figs 1 and 2, i.e. capable of generating a very high voltage.

20

In the variant according to Fig 5, it is illustrated how a transformer 31, common for the generators 1, is arranged between the parallel connection point 35 for the generators 1 and the frequency converter 34, which transformer is intended to achieve a high voltage in the part of the connection situated between the transformer and the frequency converter 34 and a comparatively lower voltage between said transformer 38 and the generators 1. This common transformer 38 is located on the wind power side of the connection 30, i.e. close to the wind power station 29. so that the main part of the connection 30 will be present between the transformer 38 and the frequency converter 34. Suitably the transformer 38 can be placed on one of the foundations for the wind power stations 29 or possibly on its own foundation on a strategic place.

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The variant in Fig 6 illustrates an alternative corresponding to the one in Fig 5 with the exception that a particular transformer 39 is here arranged for each of the generators 1. Consequently, the wind power stations are parallelly interconnected in the point
5 35 only after these transformers. In such an embodiment, it would be possible to omit the transformer 38, which has been more closely described with reference to Fig 5. Further, it is also possible to keep the transformer 38 so that the voltage from a single wind power station will be stepped up in two steps, i.e. at
10 first via the transformer 39 and then by means of the common transformer 38.

In Fig 7 a possible embodiment of the frequency converter 34 is illustrated. It here includes a direct voltage intermediate link
15 having a AC/DC-converter 40 and an inverter 41. In the direct voltage intermediate link a DC/DC-converter 42 is advantageously included. The inverter 41 is a voltage stiff self-commutated inverter. Over the DC-link of the inverter a capacitor is parallel connected. Network inductances 44 are connected in series in
20 each phase on the alternating voltage side of the inverter 41.

The inverter 41 suitably comprises an IGBT 45.

The AC/DC-converter can be built up like the inverter 41 and
25 has on its AC-side network inductances 46 in series in each phase. The converter 40 can comprise an IGBT 47. On the DC-side there is a capacitor 48 connected in parallel with the IGBT.

The plant has means (not shown) for measuring the active
30 power from the wind power plant and means for measuring the present wind speed. These measuring means are connected to a control unit comprised in the frequency converter 34, which control unit controls the frequency regulation depending on the prevailing measuring values. In that connection, the control unit
35 can be arranged to control the frequency of the connection 30 in correspondence with an ideal characteristic over the rotational

speed of the wind turbine as a function of wind speed. Such a frequency control can be denoted as "slow". It is based on that the rotational speed of the wind power stations preferably should rise linearly with the wind speed up to the maximum rotational speed. With knowledge about the wind speed, a comparatively slow frequency control can consequently take place in the connection 30 so that the most favourable conditions ensue.

The control unit is furthermore suitably arranged to control the frequency of the connection 30 by comparison of measured transmitted active power with an ideal characteristic over the rotational speed as a function of power. Such a frequency control can here popularly be denoted as "fast". It is conducted with the aim of rapid power variations and this can e.g. be achieved with PI-regulation and regeneration of the transmitted power through the DC-link, as described with reference to Fig 7.

As far as the voltage regulation in the connection 30 is concerned, this is suitable carried out in the most simple way so that the control unit is made to control the frequency converter 34 to maintain a constant ratio voltage/frequency of the connection over the major part of the frequency range.

The invention is of course not only limited to the described embodiments. Several detail modifications are consequently possible and realized by men skilled in the technical field as soon as the basic inventional idea has been presented. Such detail modifications and equivalent embodiments are included within the scope of the subsequent claims.

Claims

1. A wind power plant comprising at least one wind power station (29), which includes a wind turbine (20) and an electric generator (1) driven by this wind turbine, and an electric alternating voltage connection (30) connecting the wind power station with a transmission or distribution network (31), **characterized** in that a frequency converter (34) is connected in the alternating voltage connection (30) on the network side of the plant, which frequency converter is arranged to fix the frequency of the connection (30) between the wind power station and the converter to be substantially below the network frequency and to convert this low frequency of the connection into correspondence with the higher frequency of network.
2. A plant according to claim 1, **characterized** in that the frequency converter (34) is arranged to vary the frequency and the voltage of the connection.
3. A plant according to claim 1 or 2, **characterized** in that the frequency converter (34) is arranged to fix the frequency of the connection (30) to 20 Hz or lower, preferably within the interval 2-20 Hz.
4. A plant according to claim 2, **characterized** in that the frequency converter (34) is arranged to fix the voltage of the connection (30) to a value within the interval 10-400 kV.
5. A plant according to any of the preceding claims, **characterized** in that the frequency converter (34) comprises a direct voltage intermediate link having an AC/DC-converter (40) and an inverter (41).
6. A plant according to claim 5, **characterized** in that a DC/DC-converter (42) is comprised in the direct voltage intermediate link.

7. A plant according to claim 5 or 6, **characterized** in that the inverter (41) is a voltage stiff self-commutated inverter and that at least one capacitor (43) is connected parallelly over the DC-link of the inverter.

8. A plant according to claim 7, **characterized** in that network inductances (44) are connected in series in each phase on the alternating voltage side of the inverter (41).

9. A plant according to any of the preceding claims, **characterized** in that valves in the frequency converter (34) consist of IGBT:s connected in series.

10. A plant according to any of the preceding claims, **characterized** in that a number of generators, associated with a corresponding number of wind turbines, are parallelly interconnected on the generator side of the connection (30).

11. A plant according to any of the preceding claims, **characterized** in that the generator or generators is/are of asynchronous type.

12. A plant according to any of the preceding claims, **characterized** in that the wind turbine (20) is connected to the generator (1) via a gearing (22), preferably a single step planetary gearing.

13. A plant according to any of the preceding claims, wherein the generator (1) comprises at least one winding (7), **characterized** in that the winding is provided with a solid insulation (18).

14. A plant according to claim 13, **characterized** in that the winding comprises an insulation system comprising at least two semiconducting layers (17, 19), each of which constitutes es-

entially equipotential surfaces, and that the solid insulation (18) is located between these semiconducting layers.

5 15. A plant according to claim 14, **characterized** in that at least one of the semiconducting layers (17, 19) has essentially the same thermal coefficient of expansion as the solid insulation (18).

10 16. A plant according to any of claims 13-15. **characterized** in that the winding is formed of a high-voltage cable (7).

15 17. A plant according to any of claims 14-16, **characterized** in that the innermost (17) of the semiconducting layers has essentially the same potential as an electric conductor (14) located inwardly of this layer.

20 18. A plant according to claim 17, **characterized** in that the inner one (17) of the semiconducting layers is in electrically conducting contact with the conductor (14) or a part thereof.

19. A plant according to any of claims 14-18, **characterized** in that the outer one (19) of the semiconducting layers is connected to a potential being fixed in advance.

25 20. A plant according to claim 19, **characterized** in that the fixed potential is ground potential or otherwise a relatively low potential.

30 21. A plant according to any of the preceding claims, **characterized** in that at least one transformer (38, 39), for step-down transformation of the voltage of the connection between the generator (1) and the frequency converter (34) to a suitable generator voltage level, is arranged on the generator side of the connection (30).

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22. A plant according to claim 21, *characterized* in that the transformer (22) is common for all the occurring generators.
- 5 23. A plant according to claim 21, *characterized* in that a specific transformer (39) is arranged for each of the generators.
- 10 24. A plant according to claims 21-23, *characterized* in that each of the occurring generators has its own transformer (39) with the primary side connected to the respective generator (1) and the secondary side connected parallelly to the primary side of a further transformer (38), the secondary side of which is connected to the frequency converter (34).
- 15 25. A plant according to any of claims 23 or 24, *characterized* in that the transformer (38) being common for several generators is arranged on the generator side of the connection (30).
- 20 26. A plant according to any preceding claims, *characterized* in that the connection (30) comprises a cable (33) intended to be submerged into water, or one or several aerial lines or cables.
- 25 27. A plant according to any preceding claims, *characterized* in that it has means for measuring the active power from the wind power plant and means for measuring the present wind speed, and that these measuring means are connected to a control unit comprised in the frequency converter (34), which control unit controls the frequency regulation depending on the prevailing measuring values.
- 30 28. A plant according to claim 27, *characterized* in that the control unit is arranged to control the frequency of the connection (30) in correspondence with an ideal characteristic over rotational speed as a function of wind speed.
- 35 29. A plant according to claim 27 or 28, *characterized* in that the control unit (31) is arranged to control the frequency of the

connection by comparison of the measured transmitted active power with an ideal characteristic over the rotational speed as a function of power.

- 5 30. A plant according to any of claims 217-29, *characterized* in that the control unit is arranged to control the frequency converter to maintain a constant ratio voltage/frequency of the connection over the major part of the frequency range.
- 10 31. A method for controlling the operation of a wind power plant comprising at least one wind power station, which includes a wind turbine and electric generator driven by this wind turbine, and a electric connection connecting the generator with a transmission or distribution network, *characterized* in that a
- 15 frequency converter is connected in the electrical connection on the network side of the plant, by means of which frequency converter the frequency of the connection between the wind power station and the converter is fixed to a value being substantially below the network frequency, and that this low frequency of the
- 20 connection is converted by means of the frequency converter into correspondence with the higher frequency of the network.
32. A method according to claim 31, *characterized* in that the frequency of the connection is regulated to a value obtained by
- 25 comparison of measured wind speed with an ideal characteristic over rotational speed as a function of wind speed.
33. A method according to claim 31 or 32, *characterized* in that the frequency of the connection by means of the frequency converter is regulated based on a comparison of measured active
- 30 power with an ideal characteristic over rotational speed as a function of power.
34. A method according to any of claims 31-33, *characterized*
- 35 in that the voltage in the connection is regulated by means of the frequency converter in such a way that a constant ratio volt-

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age/frequency is maintained over the major part of the frequency range.

Abstract

A wind power plant comprising at least one wind power station (29), which includes a wind turbine and an electric generator (1) driven by this wind turbine, and an electric alternating voltage connection (30) connecting the wind power station with a transmission or distribution network (31). On the network side of the plant a frequency converter (34) is connected in the electrical alternating voltage connection (30), which frequency converter is arranged to fix the frequency of the connection between the wind power station and the converter to be essentially below the network frequency and to convert this low frequency of the connection into correspondence with the higher frequency of the network. Furthermore, the invention comprises a corresponding method for control.

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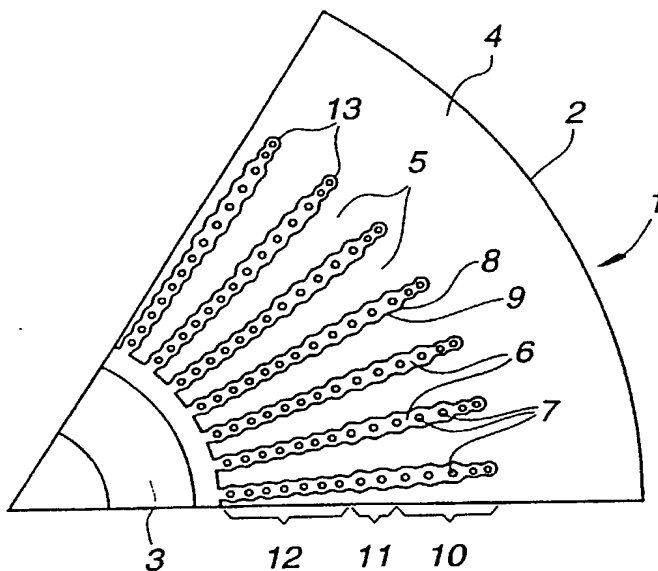


Fig. 1

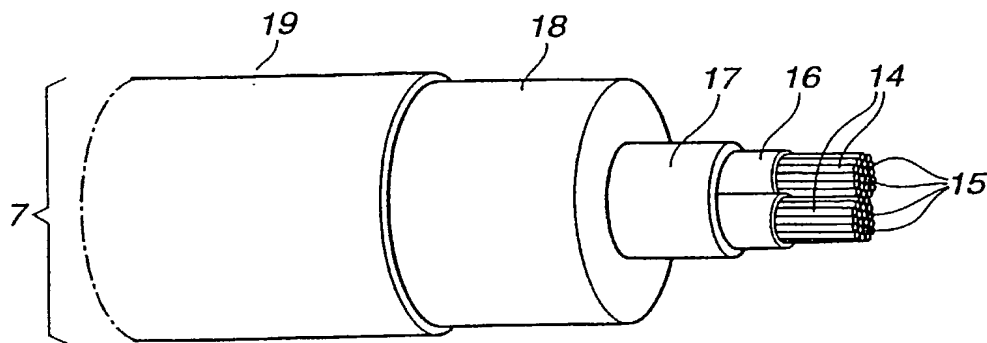


Fig. 2

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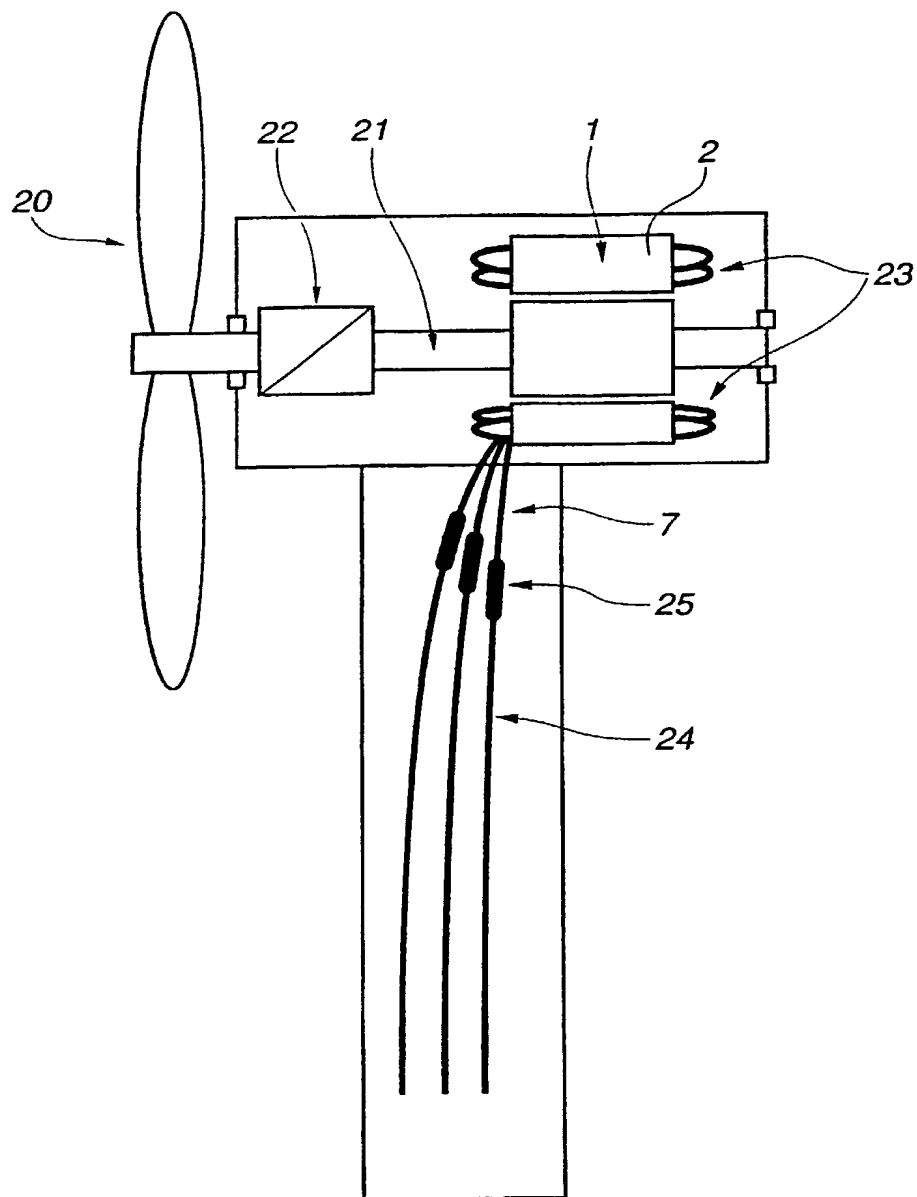


Fig. 3

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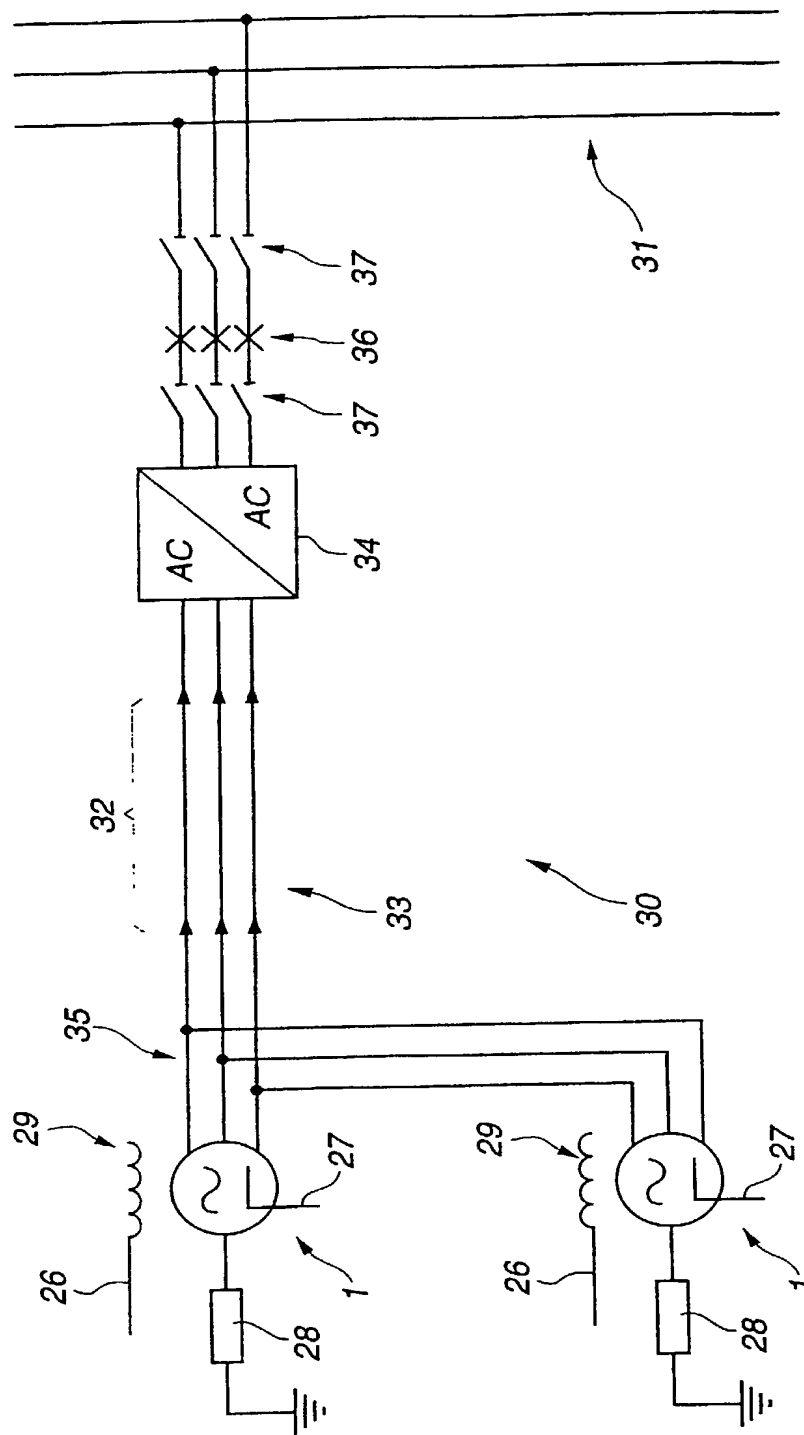


Fig. 4

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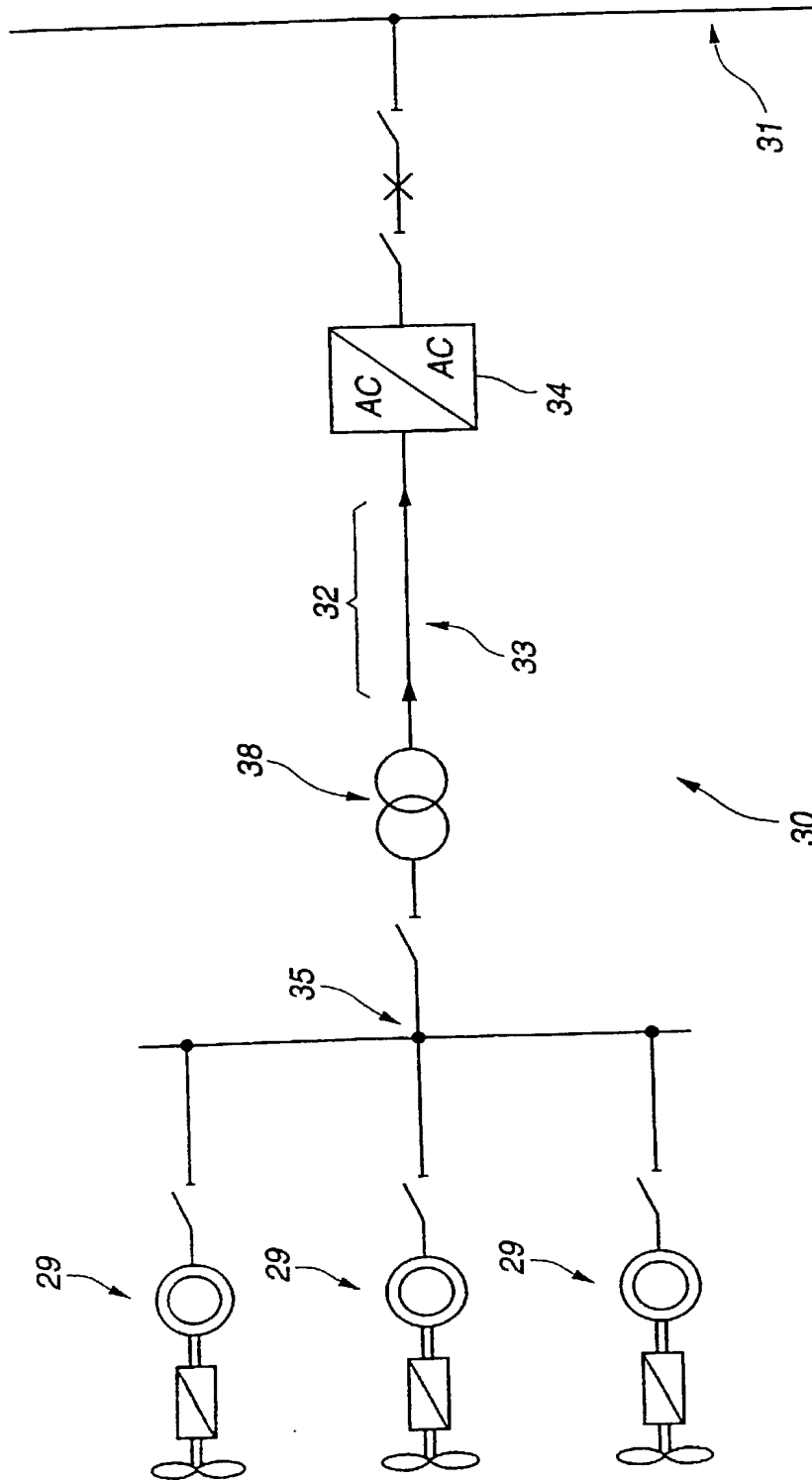


Fig. 5

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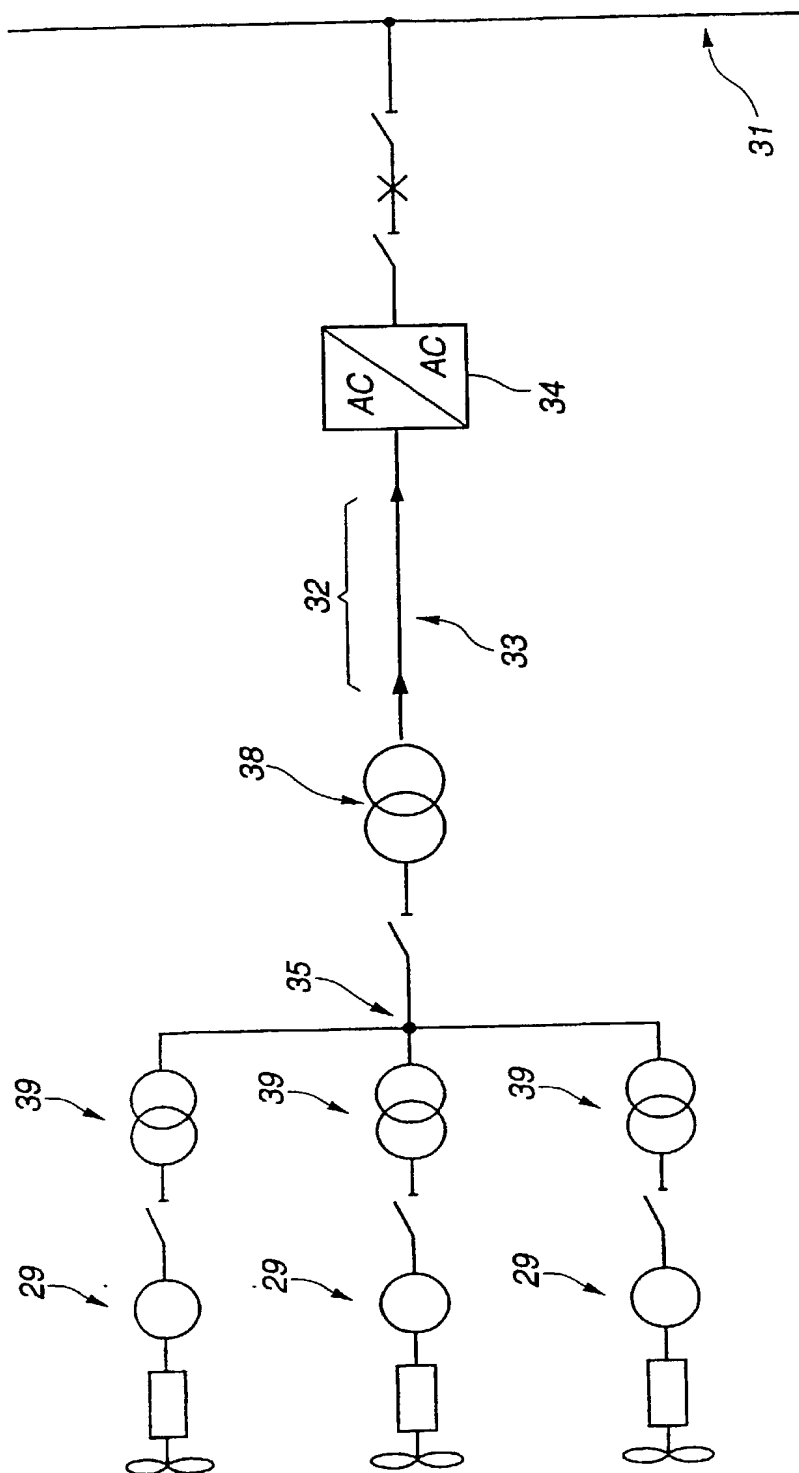


Fig. 6

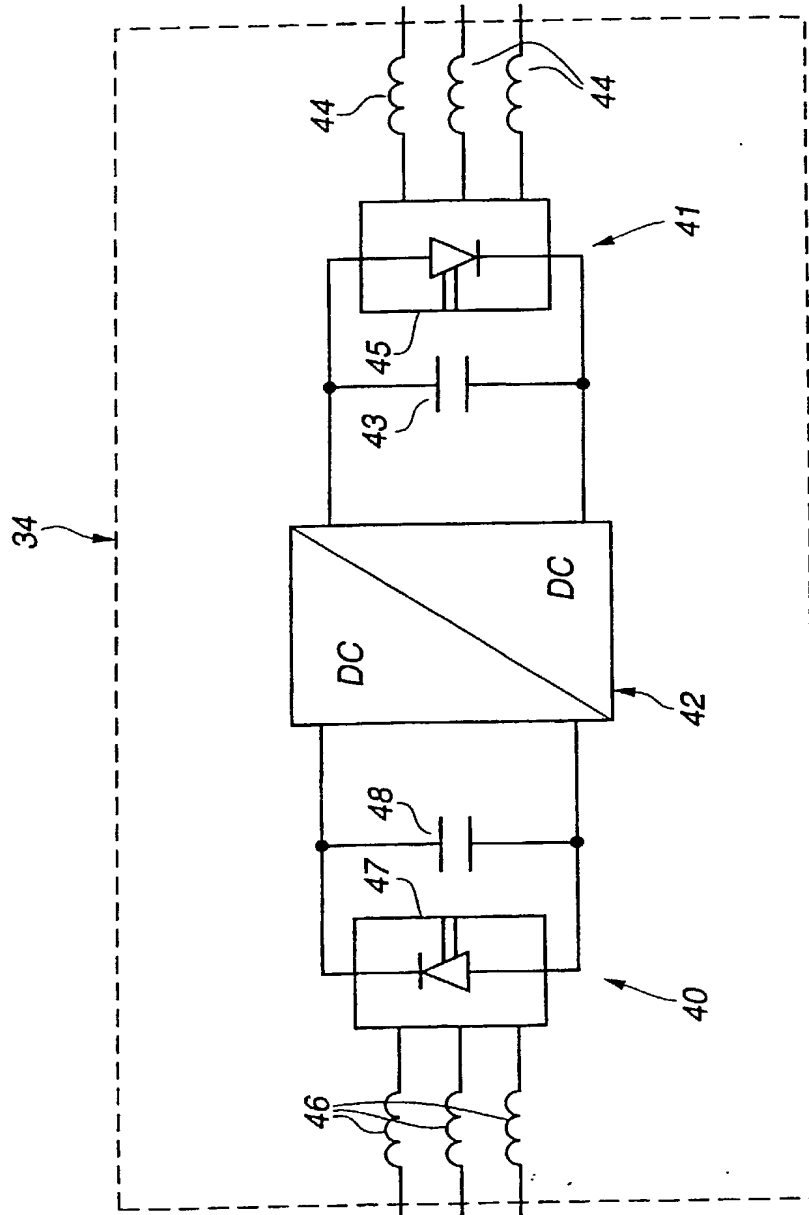


Fig. 7

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I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled.

A WIND POWER PLANT AND A METHOD FOR
CONTROL

the specification of which

☐ is attached hereto.

☒ was filed on November 26, 2001

as United States Application Number or PCT
International Application Number

09/926,608 and was amended on

_____ (if applicable)

I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims, as amended by any amendment referred to above.

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Prior Foreign Application(s)
Tidigare ansökning(ar) utomlands

(Number)
(Número)

(Country)
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(Ansökan,nr)

(Filing Date)
(ingivningsdag)

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PCT/SE99/00944

(Application No.)
(Ansökan,nr)

May 28, 1999

(Filing Date)
(ingivningsdag)

(Application No.)
(Ansökan,nr)

(Filing Date)
(ingivningsdag)

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FULLMAKT: I egenskap av uppfinnare befullmäktigat jag härmed följande advokat/er och/eller ombud att tala och svara i denna ansökan inför US Patent & Trademark Office: (Ange namn och registreringsnummer nedan)

I hereby claim foreign priority under Title 35, United States Code, § 119 (a)-(d) or 365(b) of any foreign application(s) for patent or inventor's certificate, or § 365(a) of any PCT International application which designated at least one country other than the United States, listed below and have also identified below, by checking the box, any foreign application for patent or inventor's certificate, or PCT International application having a filing date before that of the application on which priority is claimed.

Priority Claimed
Prioritetsrätt
Krävs inte

☐ Yes
Sí ☐ No
No

(Day/Month/Year Filed)
(Día/Mes/Año de presentación)

I hereby claim the benefit under Title 35, United States Code, §119(e) of any United States provisional application(s) listed below.

(Application No.)
(Ansökan,nr)

(Filing Date)
(ingivningsdag)

I hereby claim the benefit under Title 35, United States Code, § 120 of any United States application(s), or § 365(c) of any PCT International application designating the United States, listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT International application in the manner provided by the first paragraph of Title 35, United States Code, § 112, I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, § 1.56 which became available between the filing date of the prior application and the national or PCT International filing date of this application.

(Status: Patented, Pending, Abandoned)
(ärendets status: patent meddelat, ej avgjort, avslag)

(Status: Patented, Pending, Abandoned)
(ärendets status: patent meddelat, ej avgjort, avslag)

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

POWER OF ATTORNEY: As a named inventor, I hereby appoint the following attorney(s) and/or agent(s) to prosecute this application and transact all business in the Patent and Trademark Office connected therewith: (list name and registration number)

Swedish Language Declaration

**022850**

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All tel. samtal i ärendat stalls till: (namn, tel. nr.)

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| | | | |
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